

### SR 400 (I-4) Project Development and Environment (PD&E) Study FM No.: 432100-1-22-01



### **Location Hydraulic Report**

Segment 2: State Road 400 (SR 400)/Interstate 4 (I-4) from West of SR 528 (Beachline Expressway) to West of SR 435 (Kirkman Road)

Orange County (75280), Florida

August, 2016

HNTB Corporation 610 Crescent Executive Court Suite 400 Lake Mary, FL 32746



### **Professional Engineer Certificate**

I hereby certify that I am a registered professional engineer in the State of Florida practicing with HNTB Corporation, Inc., a corporation authorized to operate as an engineering business, EB#6500, by the State of Florida, Department of Professional Regulation, Board of Professional Engineers, and that I have reviewed or approved the evaluation, findings, opinions, conclusions, or technical advice hereby reported for SR 400 (I-4) Project Development and Environment Study for the Florida Department of Transportation in Orange County, Florida.

This Location Hydraulic Report (LHR) includes a summary of data collection efforts, floodplain impact estimates, limited cross drain evaluations, and an overall drainage review prepared for the conceptual analyses for the State Road 400 (SR 400)/Interstate 4 (I-4), from West of SR 528 (Beachline Expressway) to West of SR 435 (Kirkman Road) in Orange County.

I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of transportation engineering and planning as applied through professional judgments and experience. This document is for planning purposes only and is not to replace any effort required for final design.

SIGNATURE:

NAME: Sanam Rai, P.E.

FIRM: HNTB Corporation

**P.E. No.:** 69089

**DATE:** August 2016

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### 1.0 Introduction

I-4 is an integral part of Central Florida's transportation system. The Interstate carries the greatest number of people and vehicles of any transportation facility in the region and serves many of the area's primary activity centers. When the Interstate opened in February 1965, it was designed to serve intrastate and interstate travel by providing a critical link between the east and west coasts of Central Florida. Although this role continues to be a crucial transportation function of I-4, the highway has evolved to one that serves many shorter trips. Today, the highway serves as the primary link between hotel/motel complexes and tourist attractions such as Walt Disney World, Universal Studios, Sea World, the International Drive Resort Area and downtown Orlando. In addition, since I-4 is the only north-south limited access facility that is centrally located between the predominant employment centers and the major suburbs to the north, it has become the primary commuting corridor in the Central Florida metropolitan area.

Tremendous growth in Central Florida over the past decades has made it difficult for the transportation system to accommodate travel demand. A significant amount of this growth is occurring within close proximity to I-4. In recent years, congestion on I-4 has extended well beyond normal peak hours and major crashes have closed the highway, resulting in traffic congestion throughout the metropolitan area. Congestion and delays on I-4 and the parallel arterial highways are now considered to be major transportation problems facing the region. The congestion on I-4 is further evidenced by the less than desirable levels of service on the Interstate as well as the crossroads.

Projections of future population and employment in the region indicate that travel demand will continue to increase well into the future. The ability to accommodate the new travel patterns resulting from growth must be provided to sustain the region's economy. Without the improvements, extremely congested conditions are expected to occur for extended periods of time in both the morning and evening peak periods. Due to these congested conditions, user travel times will continue to increase, the movement of goods through the urban area will be slower, and the deliveries of goods within the urban area will be forced to other times throughout the day.

The need for improvements to I-4 is illustrated by the important transportation roles I-4 serves to the Central Florida region and the State of Florida. If no improvements are made to the Interstate, a loss in mobility for the area's residents, visitors, and employees can be expected, resulting in a severe threat to the continued viability of the economy and the quality of life.

This reevaluation project involves revising the original design concept showing two (2) High Occupancy Vehicle (HOV) lanes to four (4) Express Lanes as recommended in the Environmental Impact Statement (EIS) for I-4 from SR 528 to SR 472. The Express Lanes are tolled lanes and will extend the full length of the project. The access to/from the tolled lanes will be evaluated as part of this effort to determine if changes are needed from the previously approved concept for access to/from the HOV Lanes. The original I-4 PD&E Studies involved physical separation between the HOV lanes and the general use lanes on I-4. Additionally, a demand management tool was proposed during the EIS phase of the project to control the use of the lanes by requiring a minimum number of occupants per vehicle in order to maintain an acceptable level of service (Level of Service D).

This reevaluation addresses revising the demand management tool to convert the HOV lanes to tolled Express Lanes. A variable pricing tolling plan is proposed. The tolls will vary by time of day and day of week to maintain acceptable levels of service in the Express Lanes. The tolls will be collected electronically through existing E-Pass, SunPass and other systems currently in place in the Orlando metropolitan area. The conversion to Express Lanes

will maintain the same right of way limits as documented previously and will not change the impacts to the social, natural or physical environment.

A Systems Access Modification Report (SAMR) update is also being performed concurrent with the reevaluation and is expected to be completed by April 2015.

The primary objective of this Location Hydraulic Report (LHR) is to evaluate the hydraulic conditions along this proposed corridor in the existing and proposed conditions. This evaluation shall be accomplished by assessing and quantifying all floodplain impacts and providing recommendations to offset any impacts. The results of this evaluation will provide FDOT with the information necessary to reach a decision on the type, design, and location of improvements that are required for the widening of SR 400 (I-4).

This report has been prepared in accordance with the requirements set forth in Executive Order 11988, "Floodplain Management", US DOT Order 5650.2, "Floodplain Management and Protection", and Federal-Aid Policy Guide 23 CFR 650A. The intent of these regulations is to avoid or minimize roadway encroachments within the 100-year (base) floodplain, where practicable, and to avoid supporting land use development, which is incompatible with floodplain values. This report provides preliminary information on designated floodplains, cross culverts and potential floodplain impacts of the project on these areas.

General information regarding basin delineation, cross culvert location and culvert parameters used in the preparation of this report include the following:

- Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) for Orange County No. 12095C0405F AND 12095C0415F (Figure 6)
- US Department of Agriculture (USDA) Soils Conservation Service (SCS) Soils Survey for Orange County (Figure 2)
- US Geological Survey (USGS) Quadrangle Map (Figure 3)
- Florida Department of Transportation (FDOT) PD&E Manual, Part 2, Chapter 24 (revised January 2008)
- FDOT Drainage Manual (2015)
- 2014 SFWMD Basis of Review for Environmental Resource (ERP BOR)
- Existing Construction Plans
- Various Existing Permits
- Site Investigation

### 2.0 Project Description and Purpose

The Florida Department of Transportation (FDOT) is proposing to reconstruct and widen I-4 as part of the I-4 Ultimate concept. This involves the build-out of I-4 to its ultimate condition through Central Florida, including segments in Polk, Osceola, Orange, Seminole, and Volusia Counties. The concept design proposes the addition of two (2) new express lanes in each direction giving it a total of ten (10) dedicated lanes. The study area in this section from south of SR 528 (Beachline Expressway) to SR 435 (Kirkman Road) includes the interchanges at SR 528, Sand Lake Road, and at Universal Boulevard, and provides for the required stormwater treatment with seventeen (17) existing and proposed pond sites along the corridor (See Figure 1: Project Location Map). The typical section is in the process of being developed, though all efforts are being made to ensure that the design

will be contained within the existing right-of-way with the exception of the pond sites. This alignment serves as the basis for the development of the proposed improvements outlined in the Location Hydraulic Report.

### 2.1 Proposed Recommended Typical Section

The proposed roadway is intended to be an urban principal arterial interstate. The proposed improvements to I-4 include widening the existing six lane divided rural highway to a ten lane barrier separated highway. The existing roadway typical section has three 12-foot travel lanes with 10-foot shoulders in each direction. The existing right-of-way width varies but is typically 300 feet. Two mainline typical sections are proposed for I-4 Segment 2. The typical section from the begin project limits east of Central Florida Parkway to SR 528 includes a 44-foot rail envelope in the median within a minimum 300 foot right of way (6+4 with rail envelope). The typical section from SR 528 to west of SR 435 does not include the rail corridor and also has a proposed minimum 300 foot right of way (6+4 without rail envelope). Both typical sections have a design speed of 70 miles per hour (mph) and will include three 12-foot general use lanes with a 10-foot inside shoulder and a 12-foot outside shoulder (10-foot paved) and two 12-foot express lanes with a 4-foot inside shoulder and a 10-foot outside shoulder, in each direction. A barrier wall between adjacent shoulders will separate the express lanes from the general use lanes. Additionally, up to three auxiliary lanes in either direction of travel will be provided in some areas. Figure 1.2 and Figure 1.3 illustrate the proposed mainline typical sections for I-4 Segment 2.

While the overall typical section remains consistent throughout Segment 2, there are some areas along the I-4 BtU corridor that will have special sections. Special cross sections were developed to meet the needs of the project due to right of way constraints, existing utility easements or other design considerations along the corridor. These special sections may include C-D roads, braided ramp systems, elevated express lanes or elevated general use lanes. Additionally, the median width may vary in certain locations to accommodate changes in the horizontal alignment due to crossroad support structures or other design features. The special sections within the Segment 2 corridor include a C-D system between Central Florida Parkway and SR 528; the eastbound C-D Road is at grade and the westbound C-D Road is elevated. The eastbound C-D Road extends approximately 1.9 miles between SR 528 in Segment 2 and the Daryl Carter Parkway interchange located within Segment 1 of the I-4 BtU corridor. The westbound C-D Road extends approximately 5.9 miles between SR 528 in Segment 2 and the Osceola Parkway interchange located within Segment 1 of the I-4 BtU corridor.

### 3.0 Design Criteria

The design of stormwater management facilities for this project is governed by the rules and criteria set forth by the South Florida Water Management District (SFWMD) and the FDOT. These criteria were drawn from the 2014 SFWMD Basis of Review for Environmental Resource (ERP BOR) and the 2015 FDOT Drainage Manual.

### 3.1 Culvert Design

 All cross drains, if applicable, shall be designed to have sufficient hydraulic capacity to convey the 50-year (Design Frequency) storm event. All culverts shall be analyzed for the base flood (100-year).

- Backwater shall not significantly change land use values unless flood rights are purchased.
- The headwater for design frequency conditions shall be kept at or below the travel lanes.
- The highest tailwater elevation, which can be reasonably expected to occur coincident with the design storm event, shall be used (typically, crown of pipe is used).
- The minimum culvert size is 18" or its equivalent size.
- The design of all cross culverts shall comply with the guidelines set forth in the FDOT Drainage Manual, Chapter 4.

### 3.2 Floodplains/Floodways

- The proposed project may not cause a net reduction in flood storage within the 10year floodplain.
- Structures shall cause no more than a one-tenth (0.1) of a foot increase in the 100-year flood elevation 500-feet upstream.
- Proposed construction shall not cause a reduction in flood conveyance capabilities.
- Best Management Practices (BMP's) shall be employed to minimize velocity to avoid undue erosion.
- The design of encroachments shall be consistent with standards established by FEMA.

The above criteria were collected from applicable portions of:

- FDOT Drainage Handbook Culvert Design (January 2004)
- FDOT Drainage Manual (2015)
- FHWA Code of Federal Regulation 23 CFR 650A

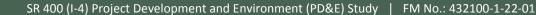




Figure 1: Project Location Map

### 4.0 Site Conditions

This project lies within the jurisdiction of the South Florida Water Management District (SFWMD). Wetlands, wildlife, soils conditions, land use, cross culverts, and floodplains describe the site conditions present within the limits of this study. Involvement within wetlands and impact of wildlife are specifically addressed in two separate

reports, "Wetlands Evaluation Report" and "Endangered Species Biological Assessment" prepared as part of this PD&E Study.

### 4.1 Soils

The Soil Survey of Orange County, Florida, published by the United States Department of Agriculture (USDA) Soil Conservation Service (SCS) has been reviewed for the project vicinity. There are eleven (11) different soil types located in the project area. Table 1 lists these soil types and their hydric properties. The Soil Survey Map for the project is illustrated in Figure 2.

**Table 1: SCS Soil Survey Information** 

Soil Type	Hydrologic Soil Group
Archbold fine sands	Α
Basinger fine sands	A/D
Candler-Apopka fine sands	Α
Immokalee fine sands	B/D
Pomello fine sand	А
Smyrna fine sand	A/D
St. Johns fine sand	B/D
St. Lucie fine sand	Α
Sanibel Muck	A/D
Smyrna-Urban land complex	A/D
Urban Land	N/A

Based on a review of the Orange County, Florida, United States Geographical Survey (USGS) quadrangle map, the existing ground surface elevations along the project alignment vary approximately from +114 to +139 feet NAVD. A reproduction of the USGS quadrangle map for the project vicinity is shown in Figure 3.

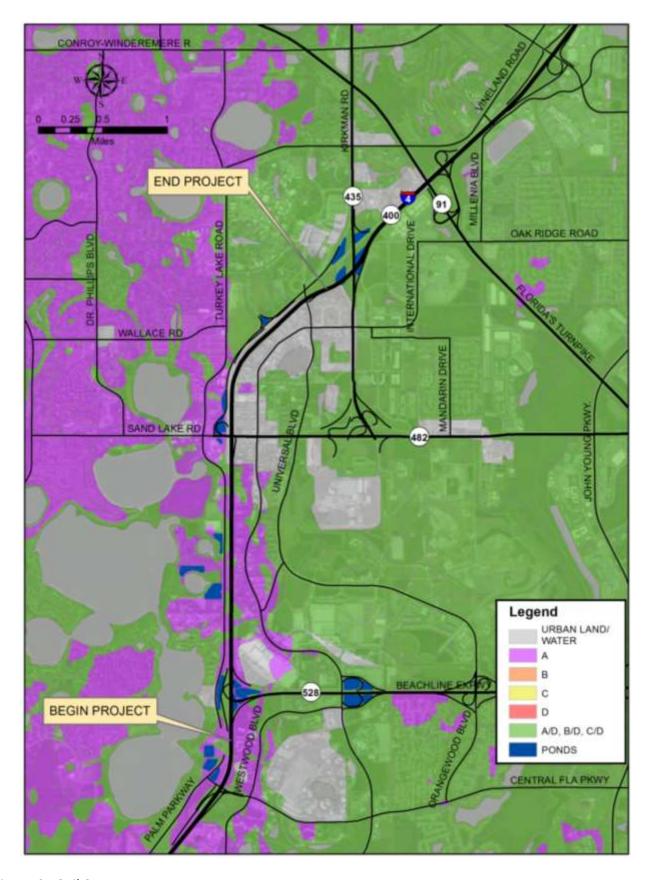


Figure 2: Soil Survey Map

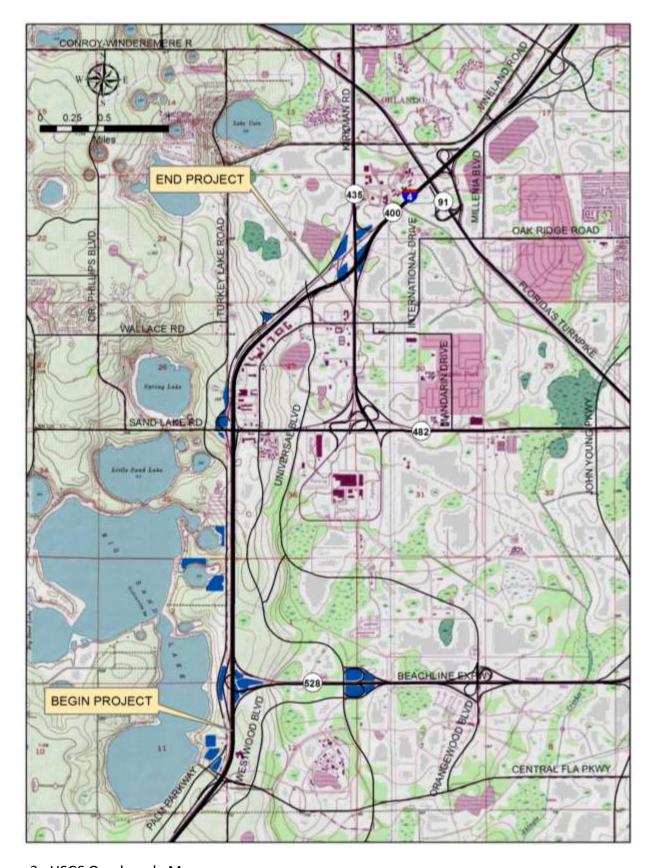


Figure 3: USGS Quadrangle Map

### 4.2 Land Use

### 4.2.1 Existing Land Use

Existing land use information within the SR 400 (I-4) PD&E Study is based on the existing land use map. The existing land uses are agricultural, acreage not zoned for agriculture, residential, retail/office, public/semi-public, vacant nonresidential and vacant residential. The majority of existing land in the study area is zoned for retail office use. Figure 4 illustrates the existing land use within the project area.

### 4.2.2 Future Land Use

Future land uses include commercial, high density residential, institutional, planned development and mixed use. The majority of future land use in the study area is zoned for mixed use. The widening of I-4 will not alter the existing or future land uses in the area. The future land uses are illustrated in Figure 5.



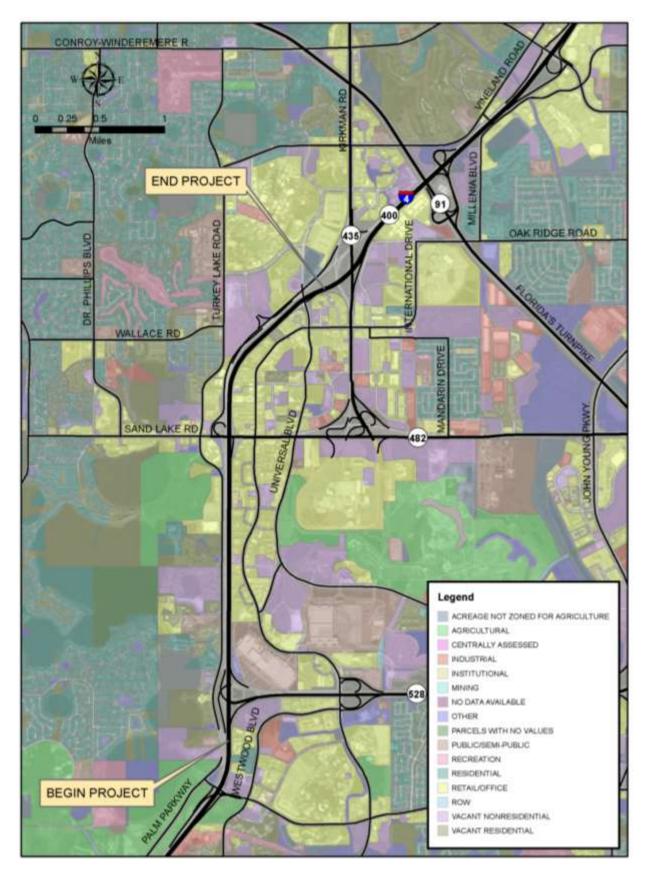


Figure 4: Existing Land Use Map

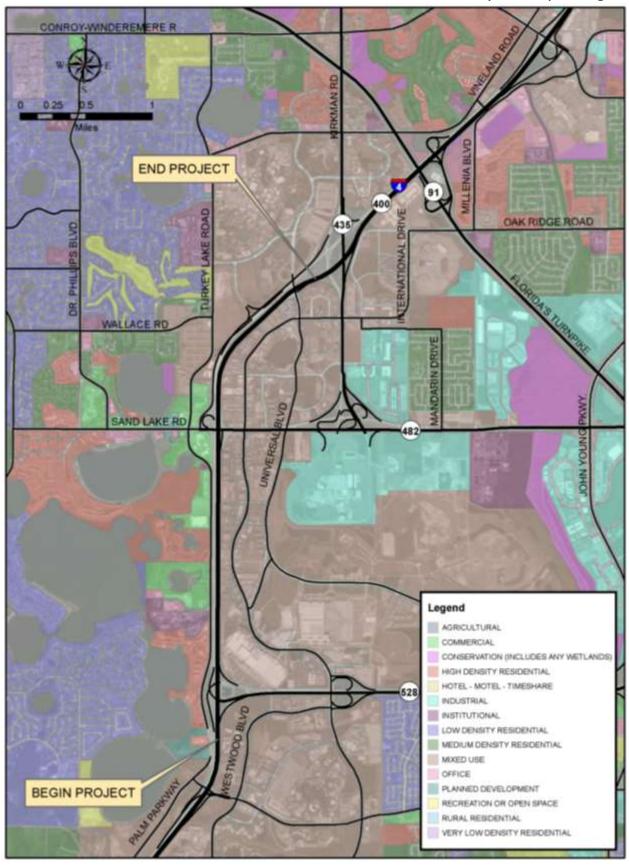


Figure 5: Future Land Use Map

### 4.3 Cross Drains

### 4.3.1 Existing Conditions

There are three (3) existing structures which act as cross drains within the study area. Table 2 depicts the existing cross drain data obtained from the Straight Line Diagram of Road Inventory (Appendix A) pertinent to the project study area, as well as, original construction plans. In the case where original construction plans were not found, cross drain invert elevations were obtained from the original PD&E study. Therefore, field verification is needed to determine the upstream and downstream flow elevations for the cross drain located at Milepost 7.409. During the design phase, field verification will be necessary to determine the actual pipe lengths as well.

**Table 2: Existing Cross Drains** 

			D	escript	ion fron	n Original Cons	truction Plan	S
Milepost	Station	Count	Span	Rise	Туре	Length (Ft)		vation NAVD)
			(in)	(in)			Upstream	Downstream
7.409	1434+46	1	42	42	RCP	230	110.49*	110.12*
8.028	1467+13	1	36	36	RCP	245	116.61	115.91
8.545	1494+90	1	30	30	RCP	228	130.81	129.11

Abbreviations: RCP – Reinforced Concrete Pipe, \*Field Verify

### 4.3.2 Proposed Conditions

Through hydraulic analysis, it was determined that all three (3) cross drains, Milepost 7.409, Milepost 8.028 and Milepost 8.545 need to be upsized. Table 3 depicts the results of the hydraulic analysis.

**Table 3: Proposed Cross Drains** 

			D	escript	ion fron	n Original Cons	truction Plan	S
Milepost	Station	Count	Span (in)	Rise (in)	Туре	Length (Ft)		vation NAVD)
			(111)	(111)			Upstream	Downstream
7.409	1434+46	1	48	48	RCP	318	110.20	110.00
8.028	1467+13	1	42	42	RCP	290	116.20	115.30
8.545	1494+90	1	36	36	RCP	285	129.30	129.10

Abbreviations: RCP – Reinforced Concrete Pipe

### 4.4 Bridge Structures

### 4.4.1 Existing Condition

There are four (4) existing bridges located within the project corridor. The first two (2) bridges are located at the interchange of SR 528 and I-4. These bridges lie within the exit ramps that cross I-4. The remaining two (2) bridges are located at Station 1480+50.00, which cross over Sand Lake

Road. Table 4 depicts the attributes of the existing bridges. Structure conditions and year of construction was provided from the original I-4 PD&E Study.

**Table 4: Existing Bridges** 

Structure No.	Milepost	Station	Description	Width (Ft)	Structure Type
750180	6.209	1371+00	SR 528 WB over I-4	31	UP
750087	6.340	1378+50	SR 528 EB over I-4	42	UP
750335	8.251	1480+50	I-4 WB over SR 482	163	BR
750336	8.251	1480+50	I-4 EB over SR 482	163	BR

Abbreviations: UP – UP (travels under facility), BR – Bridge (travels over facility)

### 4.4.2 Proposed Condition

In the proposed condition, the existing bridges will be either widened or replaced to accommodate the widening of the I-4.

### 4.5 Floodplain/Floodways

The Federal Emergency Management Agency (FEMA) has developed Flood Insurance Rate Maps (FIRM) for Orange County. According to FEMA Map Nos. 12095C0405F AND 12095C0415F, none of the roadway or the existing ponds within this segment are located in the 100-year floodplain. The proposed ponds 200-A, 200-B, 205-A and 205-B are adjacent to the 100-year floodplain, however, there is no impact to the floodplain. There are no regulatory floodways within the project corridor.

The Geographical Information System (GIS) and FEMA FIRM data identified two floodplain zones present within the project study area. These zones are identified as follows:

- Zone A Area of 1% annual chance of flood (100-year flood), no base flood elevation determined; and
- Zone AE Area of 1% annual chance of flood (100-year flood), base elevation determined.

The locations of the FEMA floodplains and the community panels referenced are shown on Figure 6.

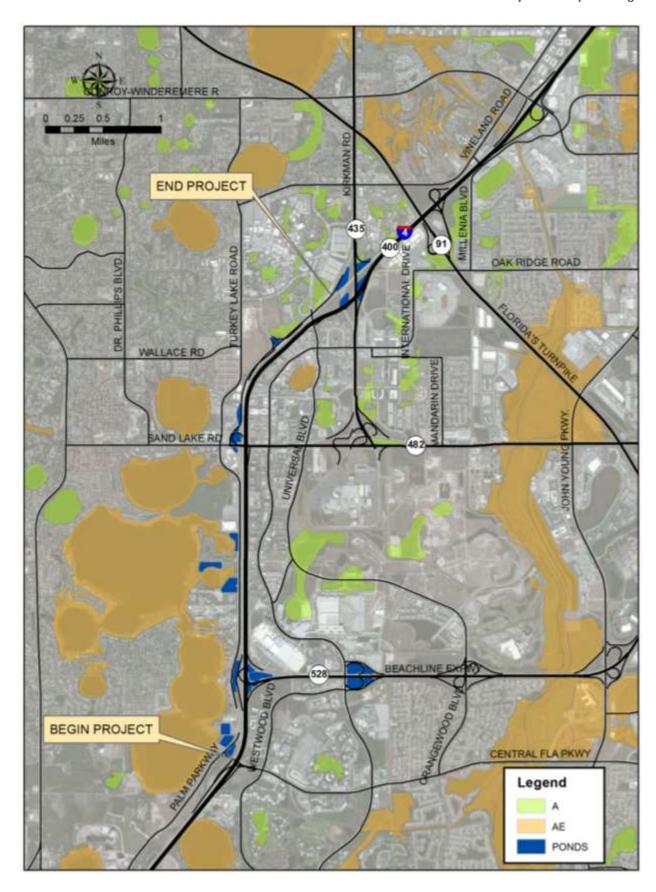


Figure 6: FEMA Flood Insurance Map

### 5.0 Recommendations and Conclusions

### **5.1 Cross Drains**

There are three (3) cross drains within the study area. The existing cross drains have been evaluated for headwater impacts to determine if replacement is necessary. Through hydraulic analysis, it was determined that all three (3) cross drains need to be upsized.

### **5.2 Bridge Structures**

There are four (4) existing bridges which will require widening. Scour analysis will not be needed during the design and construction phase, since the bridges span over I-4 and Sand Lake Road, and not water bodies.

### 5.3 Floodplains and Floodways

Floodplains are sparsely present adjacent to some proposed ponds within the study limits; however, no floodways are located within the project area. The floodplains that are present alongside of the ponds are associated lakes or conveyance to those lakes. There will be no impacts to the existing floodplains or regulatory floodways as a result of this project.

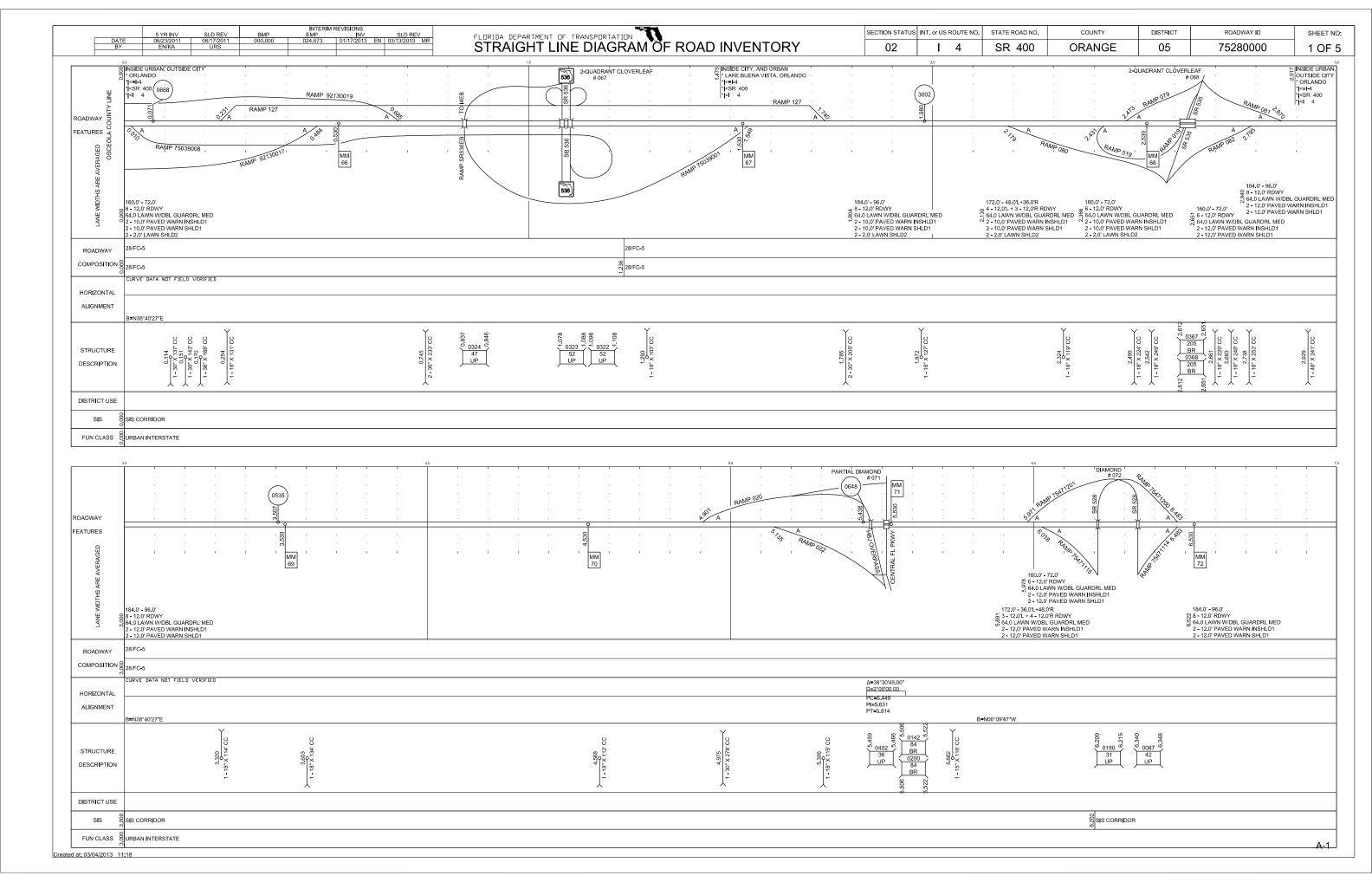
### 5.4 Project Classification

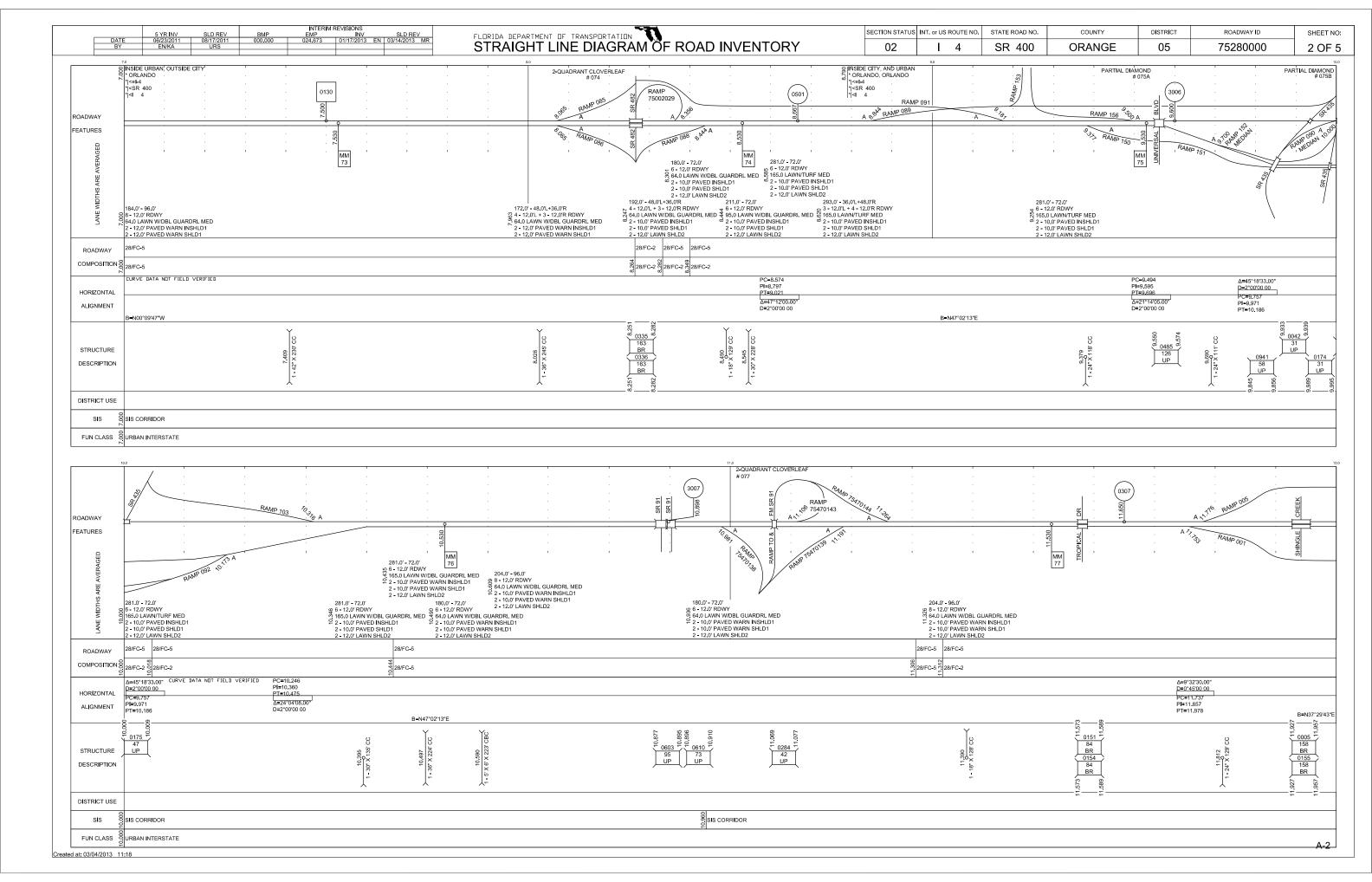
In accordance with FDOT's PD&E Manual, Part 2, Chapter 24, Section 24-2.1 "Floodplain" Statements, the proposed corridor has been evaluated to determine the impact of the proposed hydraulic modifications. Hydraulic improvements are grouped into six categories based upon the type of the hydraulic improvements and estimated floodplain impact. The proposed project can be best described as a project which will not involve any work below the 100 year flood elevation. "Although this involves work within the horizontal limits of the 100-year floodplain, no work is being performed below the 100-year flood elevation and, as a result, this project does not encroach upon the base floodplain".

### **5.5 Project Summary**

The proposed reconstruction and widening of SR 400 (I-4) involves adding two new lanes in each direction and providing stormwater management systems. There are three (3) existing culverts which will necessitate culvert replacements. This has been determined by hydraulic analysis. There are four (4) bridges within the corridor. The bridges will need to be widened to meet the proposed geometry. The proposed alignment does not impact the 100-year floodplain, nor do any proposed pond sites. By complying with regulatory criteria, the implementation of this project will not adversely affect the area adjacent to the corridor and meets the expectations of the stakeholders.

### APPENDIX A – STRAIGHT LINE DIAGRAMS





### APPENDIX B – CROSS DRAIN CALCULATIONS

## **CROSS DRAIN ANALYSIS - EXISTING CONDITION**

25-Sep-13 DATE

> LP LP S

59219

made by:
checked by:
HNTB job #:

## **HNTB** Corporation

610 Crescent Executive Court, Suite 400 Lake Mary, FL 32746

I-4 PD&E - Segment 2 PROJECT:

MP 7.409 LOCATION:

Cross Drain Characteristics:

Overtoppping El. El. 127.24

> $HW_{50} = EI. 115.57 \sum_{100} HW_{25} = EI. 114.92 \sum_{100} HW_{25} = EI.$  $HW_{100} = EI. 116.42 \overline{\Delta}$

Upstream Invert El. 110.49

0.002 ft/ft Round 110.49 0.012 3.5 ft 110.12 3.5 ft 230 ft 0.20 Entrance Loss Coef∴ Cross Drain Shape: Downstream Invert: Number of Barrels: Upstream Invert: Overtopping El.: Manning's "n": Height (D): Length (L): Slope (So): Span (B):

- Downstream Invert El. 110.12

 $\nabla$  TW<sub>50</sub> = El. 113.62

(Based on crown of pipe) 113.62 42" Pipe 127.24

Tailwater El..

Description:

 $Q_{25} = V^*A = 6 \text{ fps * } (\pi D^2/4) = 57.7 \text{ cfs}$ 

80.8 cfs  $Q_{100} = 1.4 * Q_{25} =$ 

	Į,	,	٥	, i					Headw	vater Cor	Headwater Computation							
Culvert	to #	or (	ō	Đ	<u> </u>	Inlet Control	<u>,</u>			Outlet Co	Outlet Control HW = H + DTW - LSo	= H + D.	TW - LSc			S G		Comments
Description Barrels (cfs)	Barrels	(cts)	Q	В	Q/B	Q/B HW/D* HW	MH	Ke	* *	d <sub>c</sub> ***	H**   d <sub>c</sub> ***   (d <sub>c</sub> +D)/2   TW   DTW	WT	MTG	rSo	M	≩	Velocity	
42" Pipe	τ-	27.2	35#	35#	16 49	354 354 1649 110 38	3.85	0.20	1 30	130 240	2.95	3 50	3.5	0.37	4.43	4 43	C	
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42" Pipe	-	808	4.5	3.5.4	23.09	808 35# 35# 23.09 1.52 5.32	533	0,00	280 285	285	3175	3 50	3.5	0.37	5.03	503	ΟV α	
100 Yr		;	:	:		}	1	,	) )			}	) j	 5	?	3	P o	

<sup>\*</sup> From Chart 1 of HDS-5

<sup>\*\*</sup> From Chart 5 of HDS-5
\*\*\* From Chart 4 of HDS-5

# **CROSS DRAIN ANALYSIS - PROPOSED CONDITION**

25-Sep-13 25-Sep-13

LDP F

59219

made by: checked by: HNTB job #:

DATE

### **HNTB Corporation**

610 Crescent Executive Court, Suite 400 Lake Mary, FL 32746

I-4 PD&E - Segment 2 PROJECT:

MP 7.409 LOCATION:

Cross Drain Characteristics:

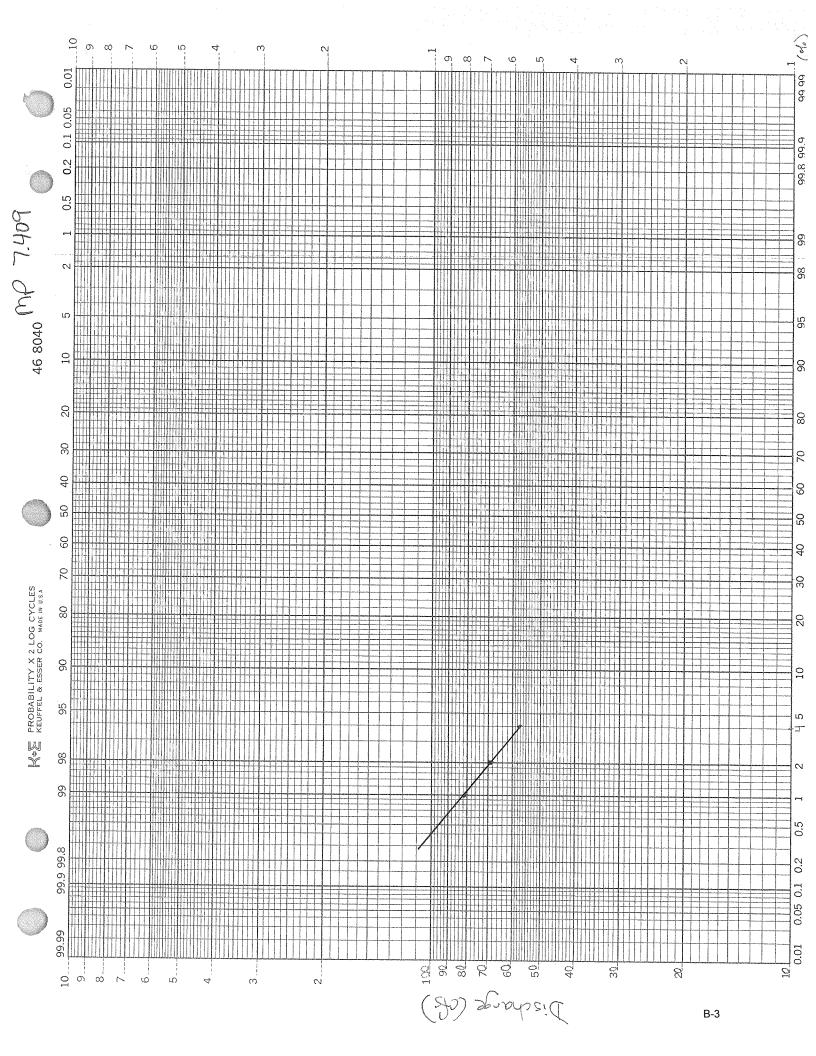
316 ft 0.001 ft/ft 110.20 110.00 127.24 113.62 48" Pipe Round 0.012 4.0 ft 4.0 ft 0.20 Entrance Loss Coef∴ Downstream Invert:
Overtopping El.:
Tailwater El.:
Description: Cross Drain Shape: Number of Barrels: Upstream Invert: Manning's "n": Height (D): Length (L): Slope (So): Span (B):

— Overtoppping El. El. 127.24	∇ TW <sub>50</sub> = El. 113.62     Downstream Invert     El. 110.00
$HW_{100} = EI. 115.17 \overline{X}$ $HW_{60} = EI. 114.72 \overline{X}$ $HW_{25} = EI. 114.42 \overline{X}$	Upstream Invert El. 110.20

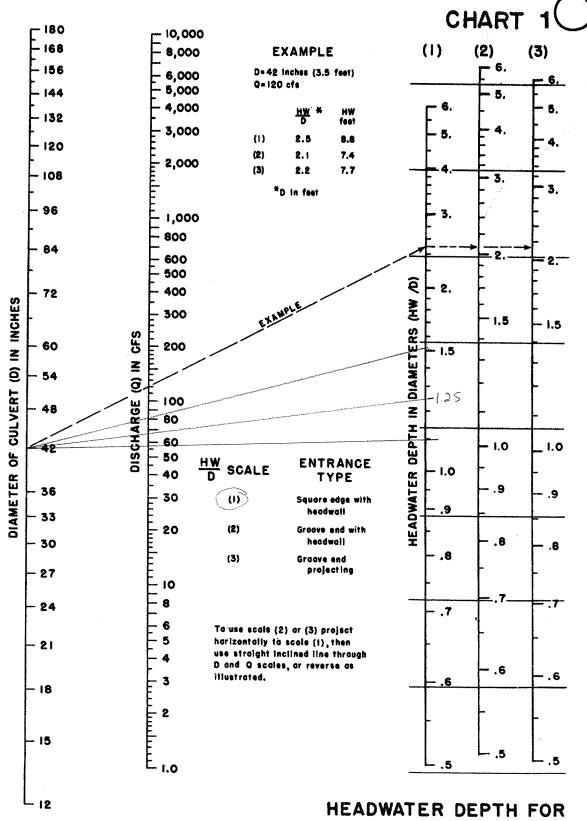
		,	ن	Cimo					Headw	ater Cor	Headwater Computation					l ,		
Culvert # of	jö #	g (	วิ	27	드	Inlet Control	_			<b>Jutlet Cc</b>	Outlet Control HW = H + DTW - LSo	H + D1	W - LSo			<u></u>	Outlet	Comments
Description Barrels (cfs)	barreis	(cts)	D	В	Q/B	Q/B HW/D* HW	ΑM	Ķe	*H	d <sub>c</sub> ***	d <sub>c</sub> ***   (d <sub>c</sub> +D)/2   TW   DTW	ΔL	DTW	LSo	HW	Ž.	Velocity	
48" Pipe	+	22.2	40#	40#	14 43	57 7 40# 40# 1443 0.85	3.40	0 20	080	230	3.15	362	3.67	0.0	4 22	4 22	4 59	
25 Yr		:	2	:	:					ì	)						3	
48" Pipe		0 69	40#	690 40# 40# 1725 0.97	17.25	0.97	3 88	0.20	1 10	2.55	3 275	367	362	0.2	4.52	4 52	5.49	
50 Yr	-		2		ì				2	3	ì			;	1	70:	<b>?</b>	
48" Pipe	·	808	40#	808 40# 40# 2020 118	20 20		4 72	020	1.55 2.70	2.70	335	367	362	0.0	4.97	497 643	6.43	
100 Yr									:	)				!			<u></u>	

<sup>\*</sup> From Chart 1 of HDS-5

<sup>\*\*</sup> From Chart 5 of HDS-5
\*\*\* From Chart 4 of HDS-5



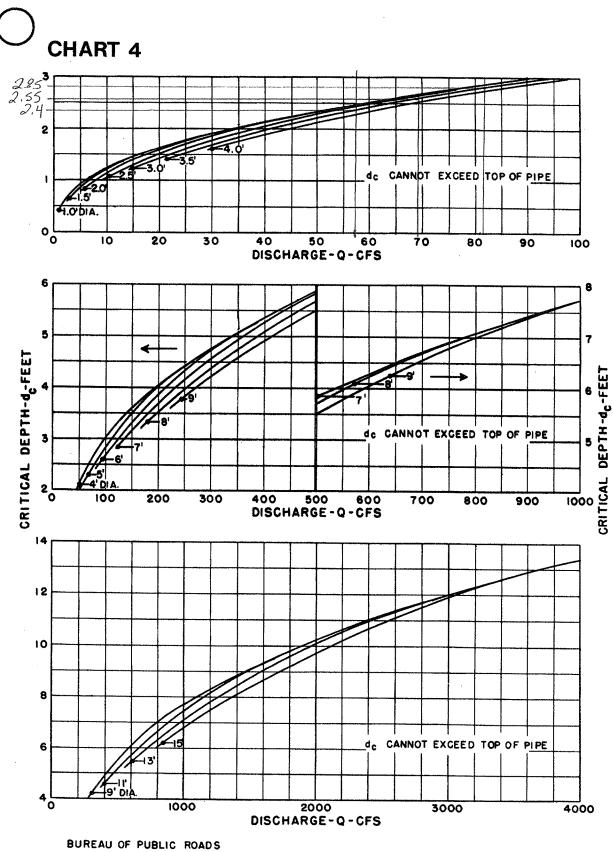
MP 7.409 (EX)



HEADWATER SCALES 283
REVISED MAY 1964

CONCRETE PIPE CULVERTS
WITH INLET CONTROL

BUREAU OF PUBLIC ROADS JAN. 1963

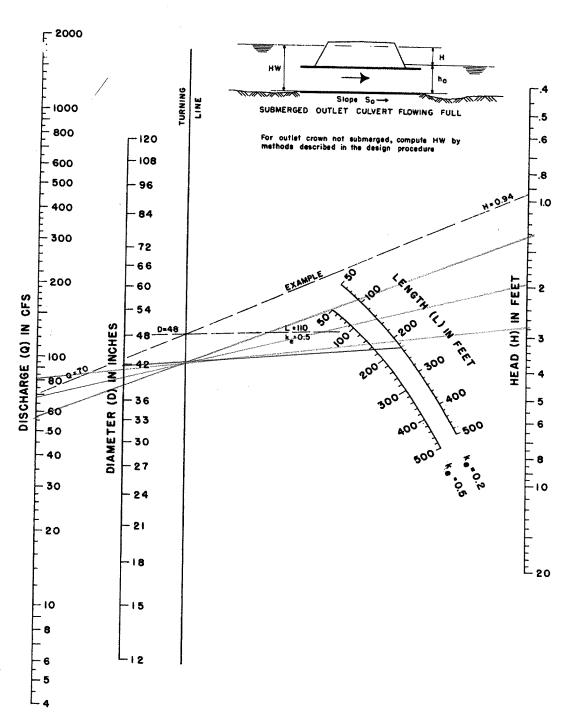


CRITICAL DEPTH CIRCULAR PIPE

JAN. 1964

MP 7.409 (EX)

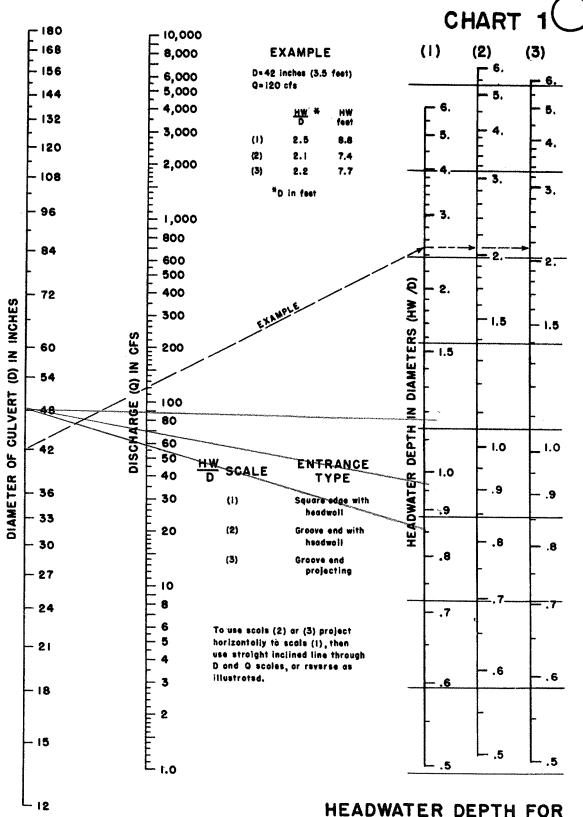




HEAD FOR
CONCRETE PIPE CULVERTS
FLOWING FULL
n = 0.012

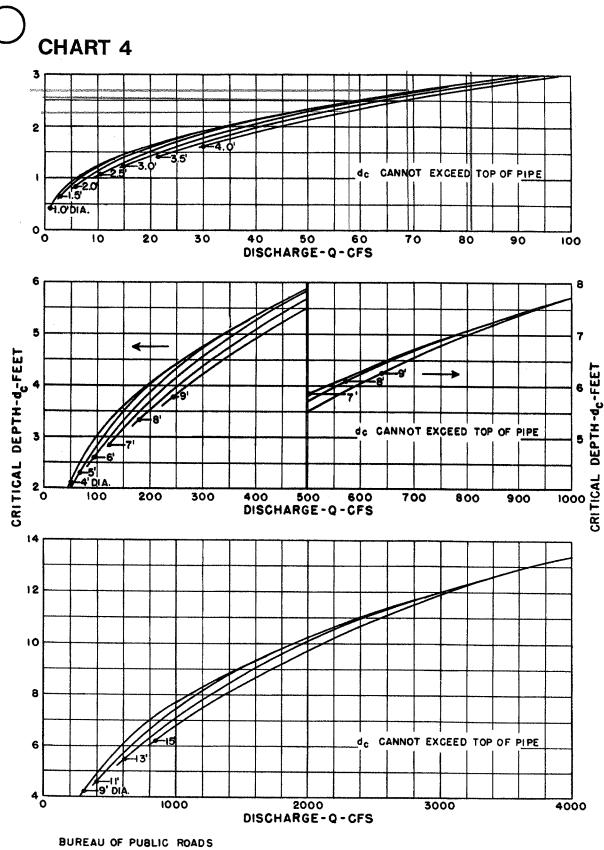
BUREAU OF PUBLIC ROADS JAN. 1963

MP 7.409 (PR)



HEADWATER SCALES 283 REVISED MAY 1964 CONCRETE PIPE CULVERTS
WITH INLET CONTROL

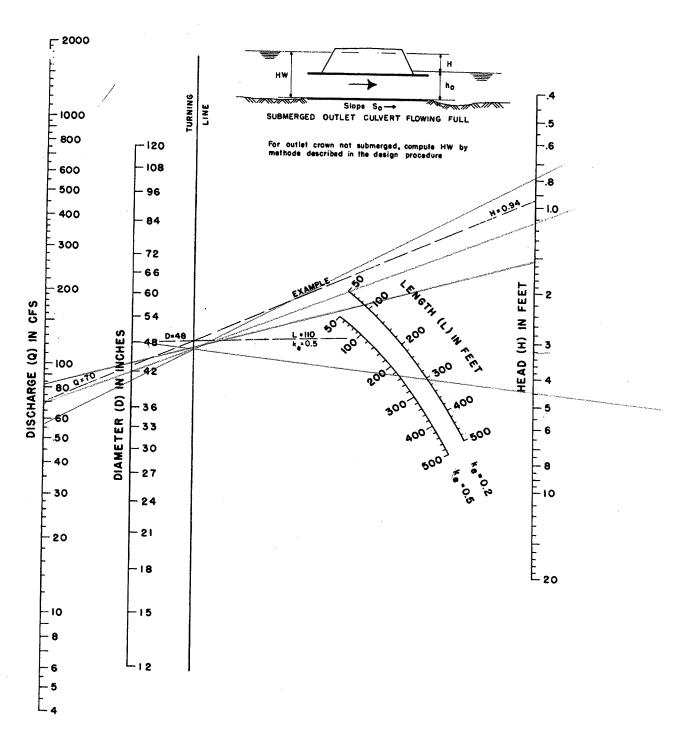
BUREAU OF PUBLIC ROADS JAN. 1963



JAN. 1964

CRITICAL DEPTH CIRCULAR PIPE





HEAD FOR CONCRETE PIPE CULVERTS FLOWING FULL n = 0.012

BUREAU OF PUBLIC ROADS JAN. 1963

## **CROSS DRAIN ANALYSIS - EXISTING CONDITION**

25-Sep-13 25-Sep-13

LDP 

made by: HNTB job #:

59219

DATE

### **HNTB Corporation**

610 Crescent Executive Court, Suite 400

Lake Mary, FL 32746

I-4 PD&E - Segment 2 PROJECT:

MP 8.028 LOCATION:

## Cross Drain Characteristics:

- Overtoppping El. El. 127.24

 $HW_{100} = EI. 121.91 \nabla$   $HW_{50} = EI. 121.13 \nabla$   $HW_{25} = EI. 120.46 \nabla$ 

0.003 ft/ft Round 0.012 3.0 ft 116.61 115.91 3.0 ft 245 ft 0.20 Entrance Loss Coef.: Cross Drain Shape: Downstream Invert: Number of Barrels: Upstream Invert: Manning's "n": Height (D): Length (L): Slope (So): Span (B):

Upstream Invert El. 116.61

> 127.24 Overtopping El.:

Downstream Invert El. 115.91

 $\sqrt{}$  TW<sub>50</sub> = EI. 118.91

(Based on crown of pipe) 36" Pipe 118.91 Tailwater El.: Description:

 $Q_{25} = V^*A = 6 \text{ fps }^* (\pi D^2/4) = 42.4 \text{ cfs}$ 59.4 cfs  $Q_{100} = 1.4 * Q_{25} =$ 

	,	(	Ö	ŭ.i.o					Headw	ater Con	Headwater Computation					(	, ;	
Culver	# d	g (	ō -	az	ī	Inlet Control	ļo			<b>Jutlet Co</b>	Outlet Control HW = H + DTW - LSo	= H + D1	rw - LSo			S :		Comments
Description Barrels (CfS)	barreis	(CIS)	Q	В	Q/B	Q/B HW/D* HW	МН	Ke	H**	d <sub>c</sub> ***	H**   d <sub>c</sub> ***   (d <sub>c</sub> +D)/2   TW   DTW   LSo	WL	WTO	LSo	HW	<b>^</b>	Velocity	
36" Pipe		42.4	3.0 ft	3.0 ft	14.14	42.4 3.0 ft 3.0 ft 14.14 1.15	3.45	0.20	1.55	1.55 2.10	2.55	3.00	8	0.7	3.85	3.85	00:9	
25 Yr																		
36" Pipe	,	51.0	30#	30#	17.00	510 30# 30# 1700 140 420		0.20	222	230	2 65	3.00	8	2.0	4 52	4 52	2.2	
50 Yr		,											,			<u> </u>		
36" Pipe	<u></u>	59.4	3.0 ft	3.0 ft	19.79	3.0 ft   3.0 ft   19.79   1.60   4.80	4 80	0.20	3.00	2.45	2,725	300	က	0.7	5.30	5.30	8.40	
100 Yr													'				!	

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Chart
From
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<sup>\*\*\*</sup> From Chart 4 of HDS-5 \*\* From Chart 5 of HDS-5

# **CROSS DRAIN ANALYSIS - PROPOSED CONDITION**

25-Sep-13 DATE

LDP

59219

made by: checked by: HNTB job #:

## **HNTB Corporation**

610 Crescent Executive Court, Suite 400 Lake Mary, FL 32746

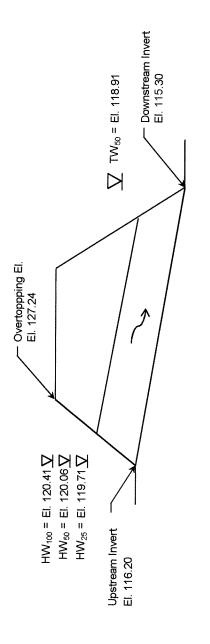
I-4 PD&E - Segment 2

PROJECT:

MP 8.028 LOCATION:

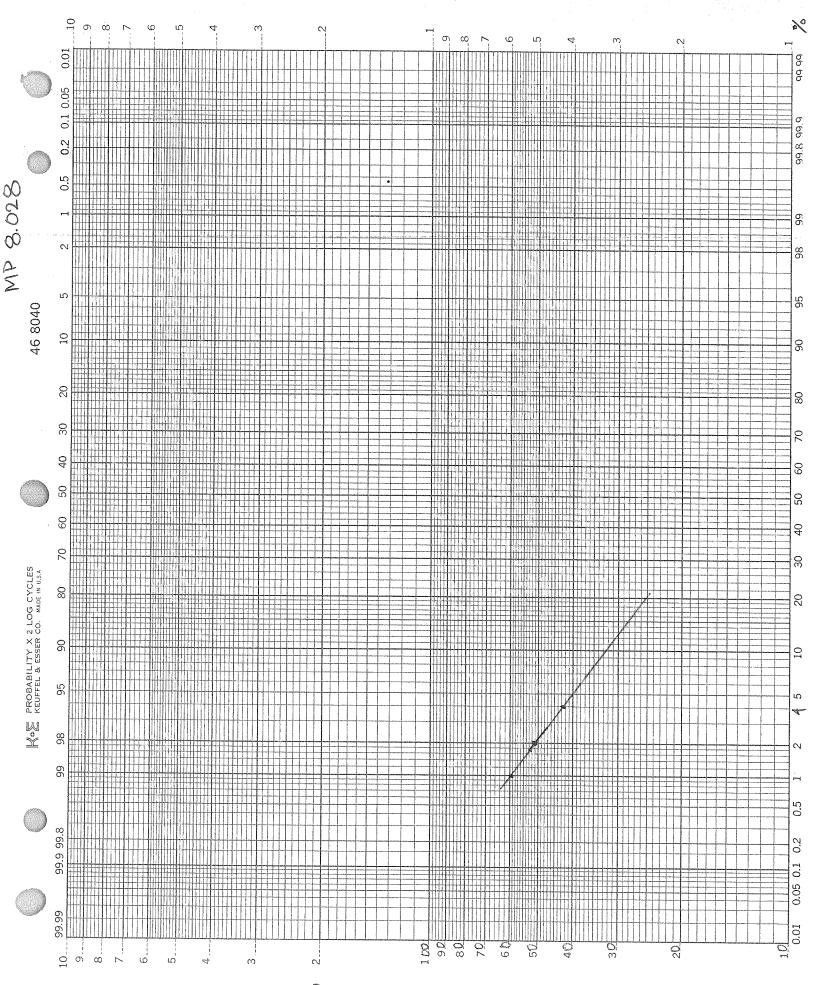
## Cross Drain Characteristics:

<b>-</b>	Round	0.012	0.20	3.5 ft	3.5#	300 ft	0.003 ft/ft	116.20	115.30	127.24	118.91	42" Pipe
Number of Barrels:	Cross Drain Shape:	Manning's "n":	Entrance Loss Coef.:	Span (B):	Height (D):	Length (L):	Slope (So):	Upstream Invert:	Downstream Invert:	Overtopping El.:	Tailwater El∴	Description:

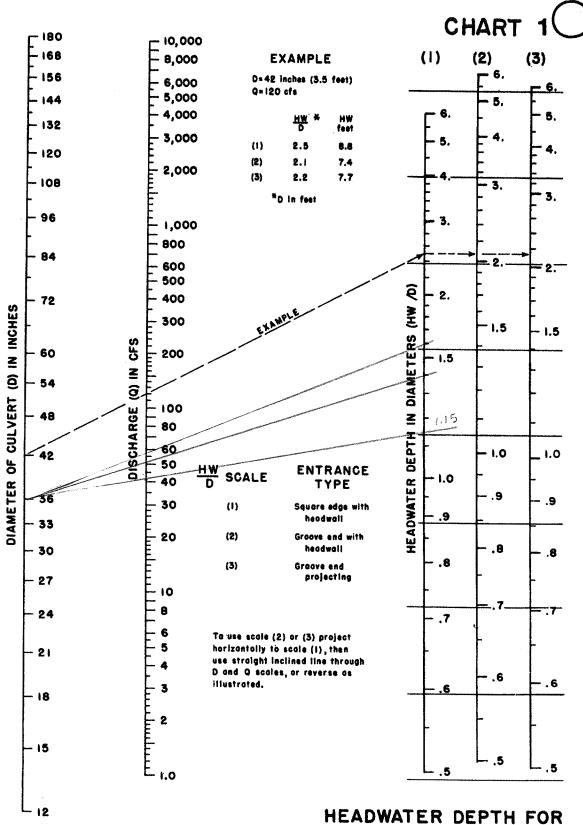


	,	,	0	O.i.o					Headw	vater Cor	Headwater Computation							
Cullvert # or	ا # ق	<b>3</b> {	?	27		Inlet Control	-0			Outlet Co	Outlet Control HW = H + DTW - LSo	- H + D1	W-LSc			Co	Outlet	Comments
Description barreis (crs)	barreis	(crs)	Ο	В	Q/B	Q/B HW/D* HV	МН	Ke	*H	d <sub>c</sub> ***	H**   d <sub>c</sub> ***   (d <sub>c</sub> +D)/2   TW   DTW   LSo	ΔL	WTO	LSo	MH.	<u>}</u>	Velocity	
42" Pipe	,	424	35#	35#	12.12	424 35# 35# 1212 088	3.08	0.20	0.80	00 6	27.6	3.61	361	0	251	2 51	7	
25 Yr										j	 ) i	- ) )		) j		5	F F	
42" Pipe	,	51.0	35#	35#	14.57	510 35# 35# 1457 105	3,68	20	7 1 2	225	2875	2	20	0	386	28.6	200	A LEAN AND AND AND AND AND AND AND AND AND A
50 Yr	-			:	-	2			<u>.</u>	3	) j		 ) )	?	3	3	3	
42" Pipe	·	59 4	35#	594 35# 35#	16.96	1 15	4.03	020	150 240	2.40	2 95	2 61	200	σ	10.4	2.2	77	
100 Yr									)	<u>.</u> i	} i		 5	) j	- !		 5	

<sup>\*</sup> From Chart 1 of HDS-5
\*\* From Chart 5 of HDS-5
\*\*\* From Chart 4 of HDS-5



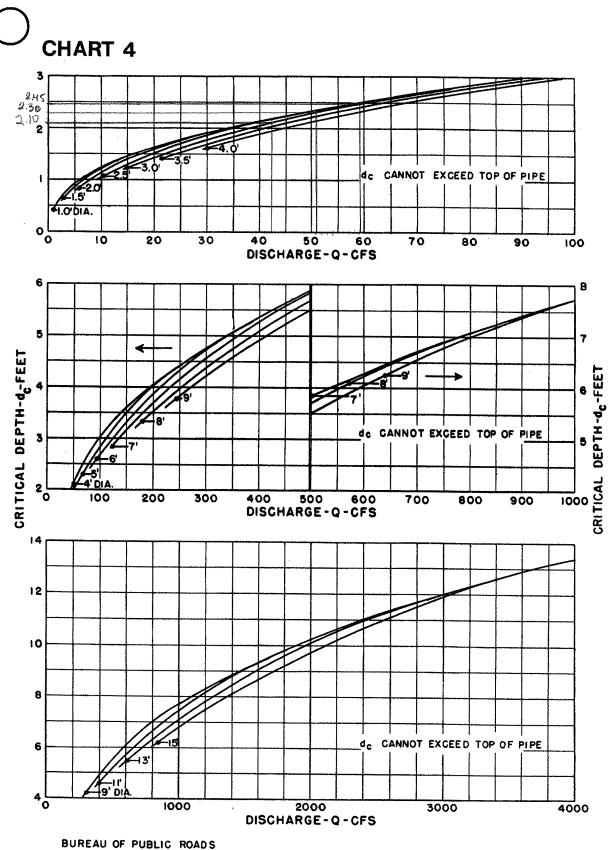
Discharge (cfs)



HEADWATER SCALES 283

REVISED MAY 1964 BUREAU OF PUBLIC ROADS JAN. 1963

CONCRETE PIPE CULVERTS WITH INLET CONTROL

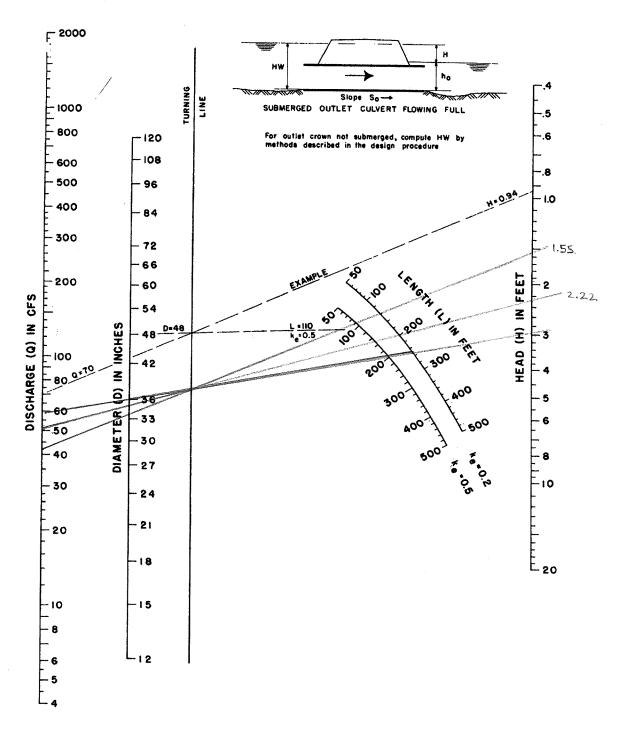


BUREAU OF PUBLIC ROADS
JAN. 1964

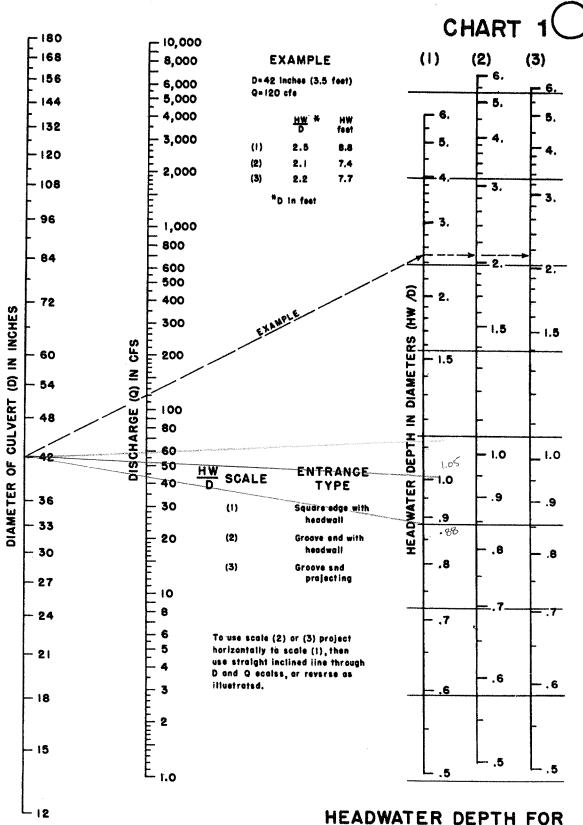
CRITICAL DEPTH CIRCULAR PIPE

MP 8.028 (Ex)

#### CHART 5

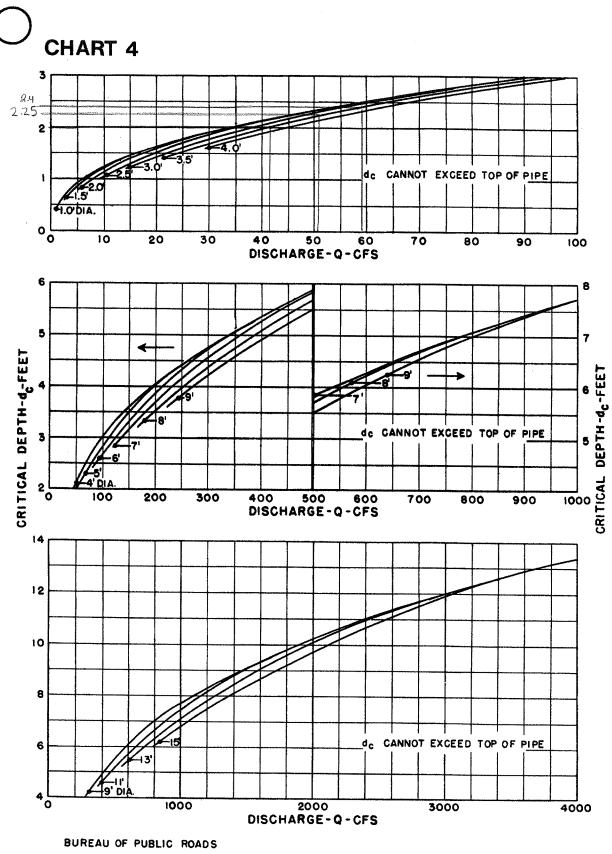


HEAD FOR
CONCRETE PIPE CULVERTS
FLOWING FULL
n = 0.012



HEADWATER SCALES 283 REVISED MAY 1964

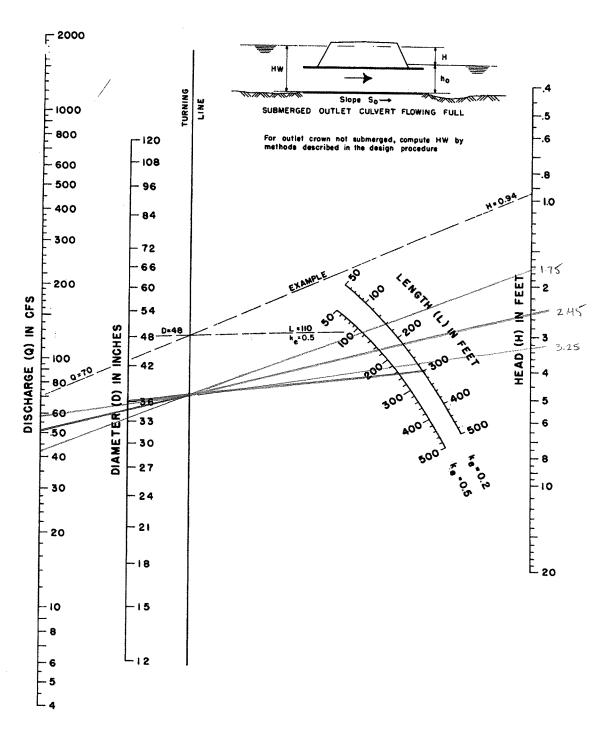
CONCRETE PIPE CULVERTS
WITH INLET CONTROL



JAN. 1964

CRITICAL DE PTH CIRCULAR PIPE





HEAD FOR
CONCRETE PIPE CULVERTS
FLOWING FULL
n = 0.012

## **CROSS DRAIN ANALYSIS - EXISTING CONDITION**

25-Sep-13 25-Sep-13

LDP 3

made by: HNTB job #:

59219

DATE

#### **HNTB** Corporation

610 Crescent Executive Court, Suite 400 Lake Mary, FL 32746

I-4 PD&E - Segment 2 PROJECT:

MP 8.545 LOCATION:

Cross Drain Characteristics:

Overtoppping El. El. 137.56

 $HW_{100} = EI. 135.31 \sum$   $HW_{50} = EI. 134.56 \sum$   $HW_{25} = EI. 133.94 \sum$ 

Upstream Invert El. 130.81

Round 0.012 2.5 ft 2.5 ft 228 ft 0.20 Entrance Loss Coef.: Cross Drain Shape: Downstream Invert: Number of Barrels: Upstream Invert: Manning's "n": Slope (So): Height (D): Length (L): Span (B):

0.007 ft/ft 130.81

Downstream InvertEl. 129.11

 $\sqrt{}$  TW<sub>50</sub> = EI. 131.61

129.11 Overtopping El.:

(Based on crown of pipe) 137.56 30" Pipe 131.61

Tailwater El.:

Description:

 $Q_{25} = V^*A = 6 \text{ fps }^* (\pi D^2/4) = 29.5 \text{ cfs}$ 

41.2 cfs  $Q_{100} = 1.4 * Q_{25} =$ 

	Comments							
, ,	Conflet	Velocity	6.00		717		8.40	
(	S	λ L	3.13		3.75		4.50 8.40	
		HW	2.60		3.20		4.20	
		LSo	1.7		1.7		7.1	
	LW - LS	DTW	2.5		2.5		2.5	
	_O + H =	WL	2.50		2.50		2.50	
Headwater Computation	Outlet Control HW = H + DTW - LSo	$H^{**}$   $d_c^{***}$   $(d_c+D)/2$   TW   DTW   LSo	2.2		2.25		2.35	
vater Cor	Outlet Co	d <sub>c</sub> ***	1.90		2.00		2.20	
Headv		**H	1.80		0.20 2.40			
		Кe	0.20		0.20		0.20 3.40	
	ō	МH	3.13		3.75		4.50	
	Inlet Contro	Q/B HW/D*	1.25		1.50		98	
	드	Q/B	11.78 1.25		14.08 1.50		41.2 2.5 ft 2.5 ft 16.49 1.80	
Orio	97	В	2.5ft 2.5ft		2.5 ft 2.5 ft		2.5 ft	
:0	ō	۵	2.5 ft		2.5 ft		2.5 ft	
Ĭ	<b>ઝ</b> (	(cts)	29.5		35.2		41.2	
	to '	Barrels	_		-			
	Culvert	Description Barrels (cfs)	30" Pipe	25 Yr	30" Pipe	50 Yr	30" Pipe	100 Yr

<sup>\*</sup> From Chart 1 of HDS-5

<sup>\*\*\*</sup> From Chart 4 of HDS-5 \*\* From Chart 5 of HDS-5

# **CROSS DRAIN ANALYSIS - PROPOSED CONDITION**

25-Sep-13 25-Sep-13 DATE

> P -H

59219

made by:
checked by:
HNTB job #:

### HNTB Corporation

610 Crescent Executive Court, Suite 400 Lake Mary, FL 32746

I-4 PD&E - Segment 2 PROJECT:

MP 8.545 LOCATION:

Cross Drain Characteristics:

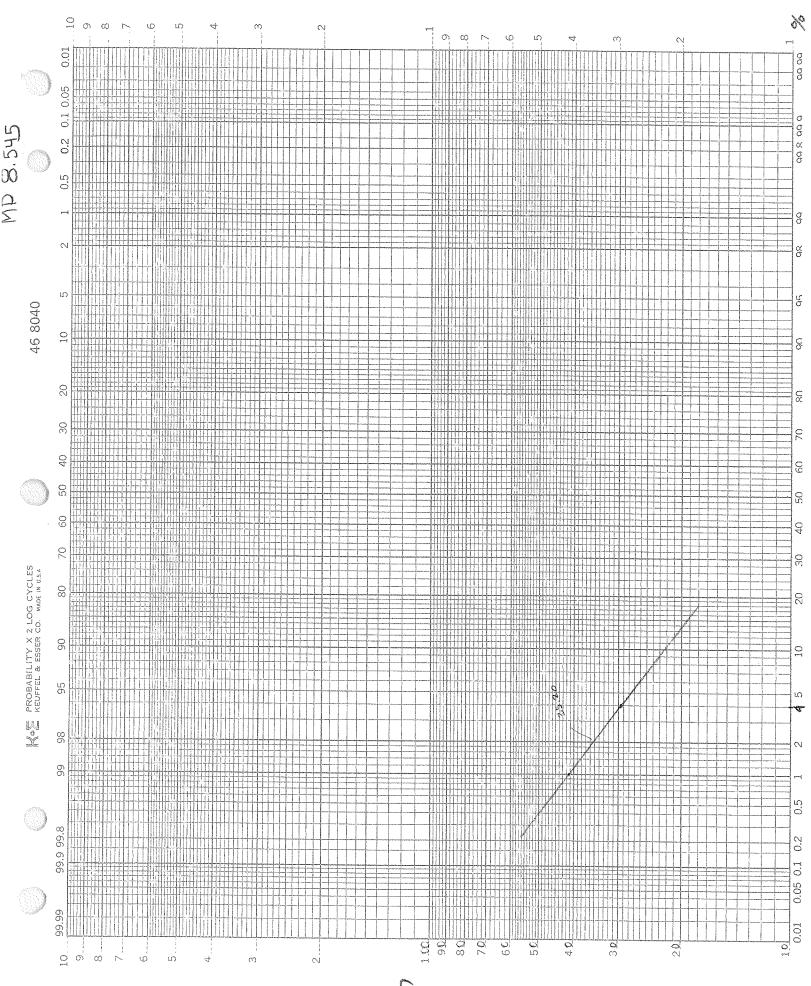
283 ft 0.0007 ft/ft 129.30 129.10 137.56 Round 0.012 3.0 ft 3.0 ft 0.20 Entrance Loss Coef.: Cross Drain Shape: Downstream Invert: Number of Barrels: Overtopping EI.: Tailwater EI.: Description: Upstream Invert: Manning's "n": Height (D): Length (L): Slope (So): Span (B):

131.61 36" Pipe

Overtoppping EI. EI. 137.56	TW <sub>50</sub> = El. 131.61  Downstream Invert El. 129.10
$HW_{100} = EI. 133.15 \overline{\Sigma}$ $HW_{50} = EI. 132.71 \overline{\Sigma}$ $HW_{25} = EI. 132.41 \overline{\Sigma}$	Upstream Invert El. 129.30

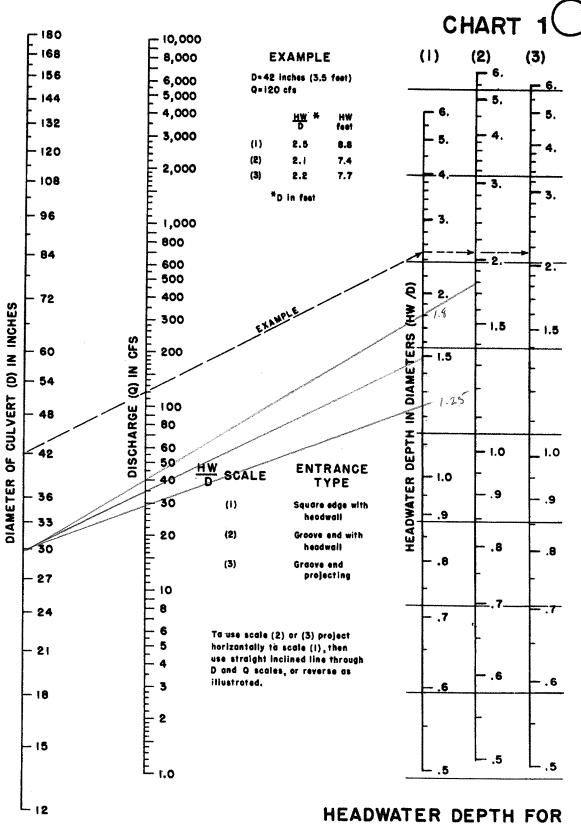
		Ğ	٥	Š					Headv	vater Co	Headwater Computation					(		
Culvert # of C	to # (	g (	ñ	217E	4	Inlet Control	rol		-	Outlet C	Outlet Control HW = H + DTW - LSo	= H + D.	TW - LSo			5	Con. Outlet	Comments
Description Barrels (cfs)	Barrels	(cfs)	D	В	Q/B	Q/B HW/D* HW	МΗ	Ke	**H	d <sub>c</sub> ***	H**   d <sub>c</sub> ***   (d <sub>c</sub> +D)/2   TW   DTW   LSo	MΤ	MTQ	LSo	HW	Λ	velocity	
36" Pipe		29.5	295 3.0 ft 3.0 ft 9.82	3.0#	9.82	0.88 2.64	2.64	0.20	0.80	0.80 1.80	2.4	2.51	2.51 2.51	0.2	3.11	3.11	4.17	
25 Yr																		
36" Pipe		35.2	3.0 ft	30#	11.73	352 30# 30# 1173 1.00 3.00	3.00	0.20		1.10 1.90	2.45	2.51	2.51 2.51 0.2		3.41	3.41	4.98	
50 Yr	•	}	:												_			
36" Pipe		41.2	3.0	30#	13.74	412 304 304 1374 112 336	3 36	0 20	0.20 1.50	2 10	2.55	2.51	2.55	0.0	3 85	3.85	5 83	
100 Yr		!		:														

<sup>\*</sup> From Chart 1 of HDS-5
\*\* From Chart 5 of HDS-5
\*\*\* From Chart 4 of HDS-5



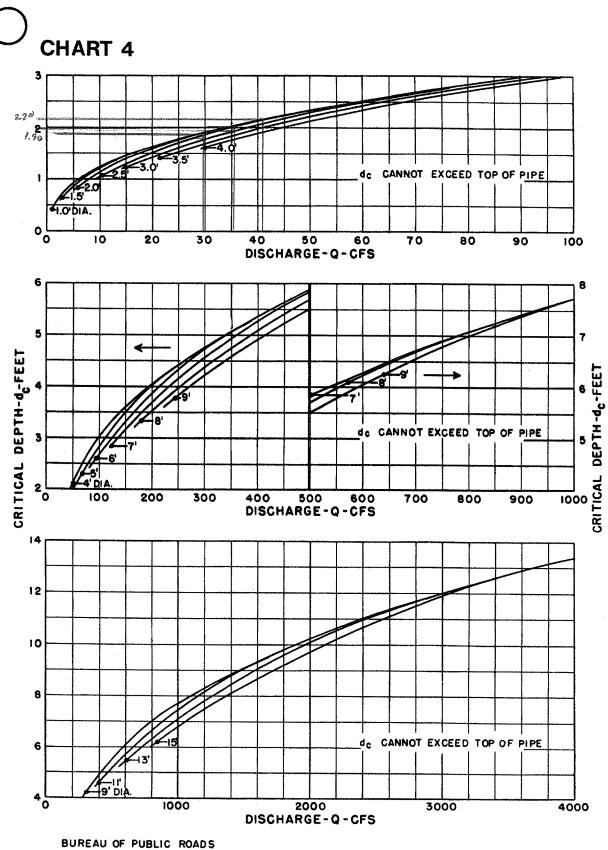
Discharge (cfs)

B-23



HEADWATER SCALES 283
REVISED MAY 1964

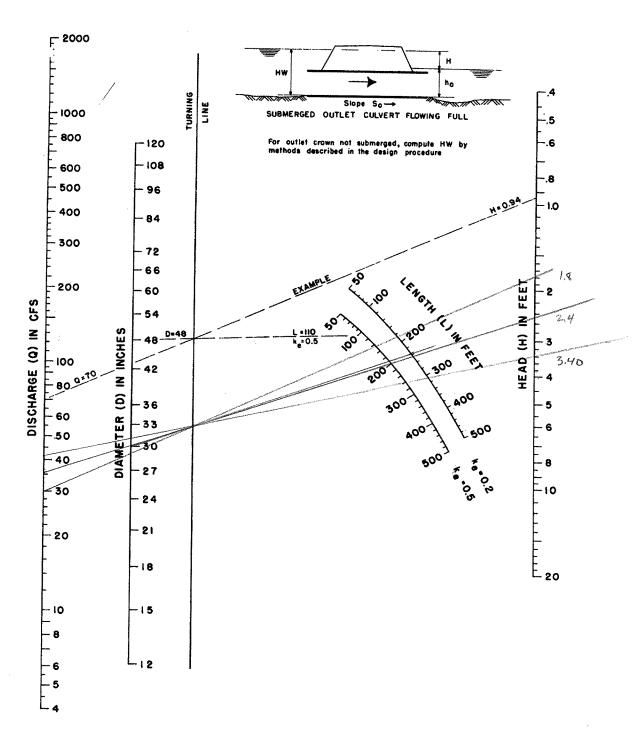
HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL



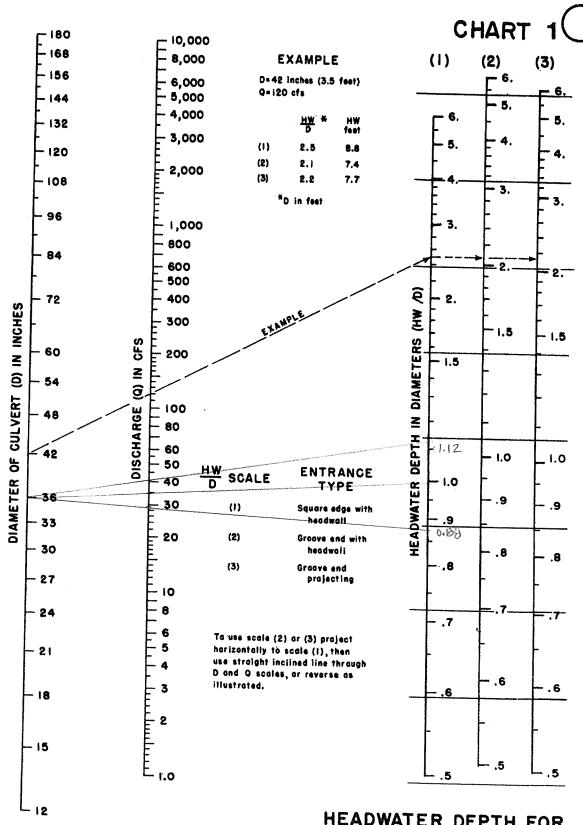
CRITICAL DEPTH CIRCULAR PIPE

JAN. 1964



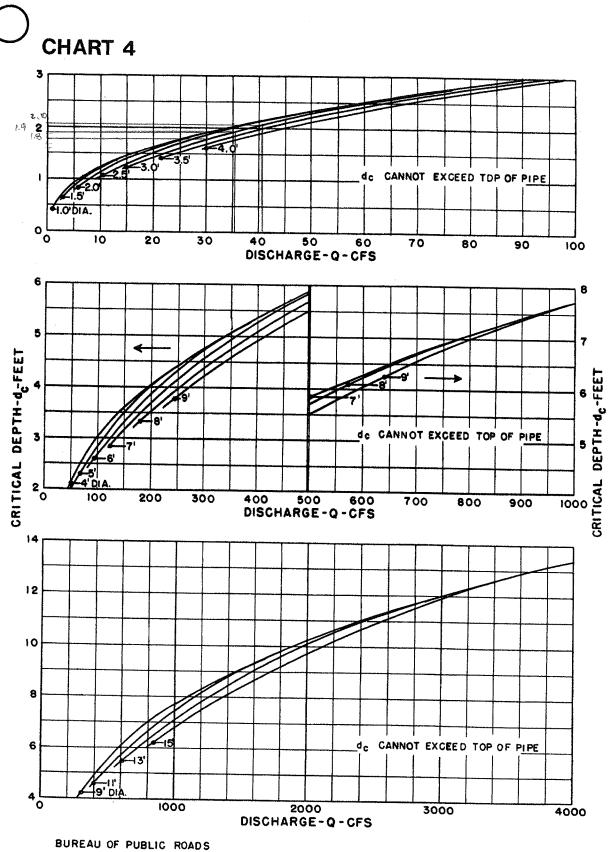


HEAD FOR
CONCRETE PIPE CULVERTS
FLOWING FULL
n = 0.012



HEADWATER SCALES 283
BUREAU OF PUBLIC ROADS JAN. 1963 REVISED MAY 1964

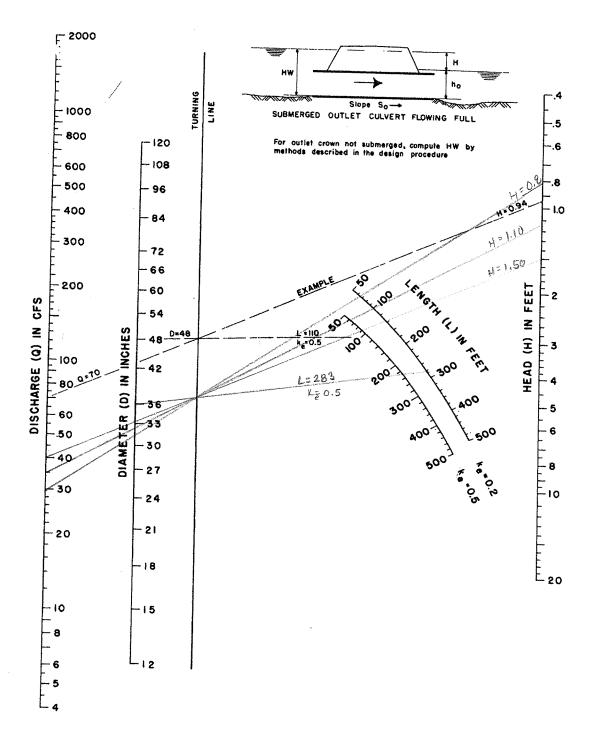
HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL



BUREAU OF PUBLIC ROADS JAN. 1964

CRITICAL DEPTH CIRCULAR PIPE





HEAD FOR
CONCRETE PIPE CULVERTS
FLOWING FULL
n = 0.012